

Case Study: Successfully Designing, Installing, and Testing a Microgrid

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Chronological History of Microgrids

- Microgrid projects
- Lessons learned
- Technology advancements
- Remaining challenges

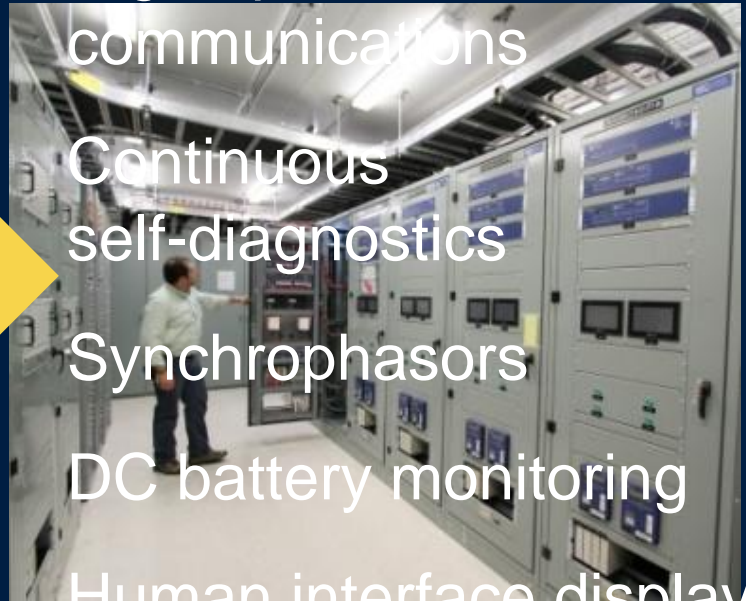
1984–2004 Microgrid Intelligence

Multifunction Microprocessor Relays Evolve Rapidly

- Multifunction protection
- Remote I/O
- Metering
- Power quality monitoring
- Programmable logic controller
- IEC 61850
- Sequence of Events records

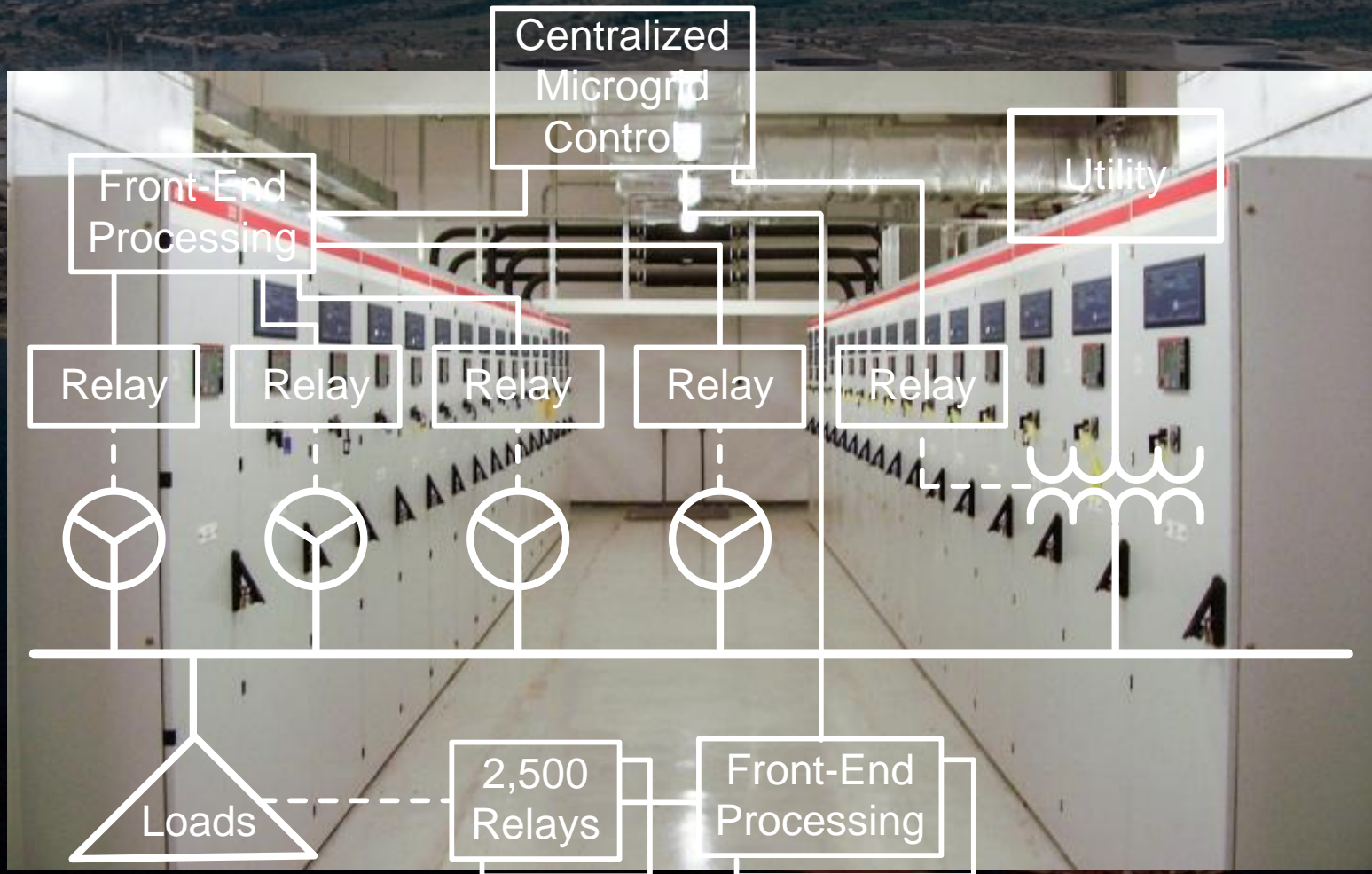


- High-speed communications
- Continuous self-diagnostics
- Synchrophasors
- DC battery monitoring
- Human interface displays
- Trip and close controls
- Oscillography recorder



2002 – Motor Oil Hellas

Korinthos, Greece



2002 – Motor Oil Hellas

Speed Is Essential for Seamless Islanding!

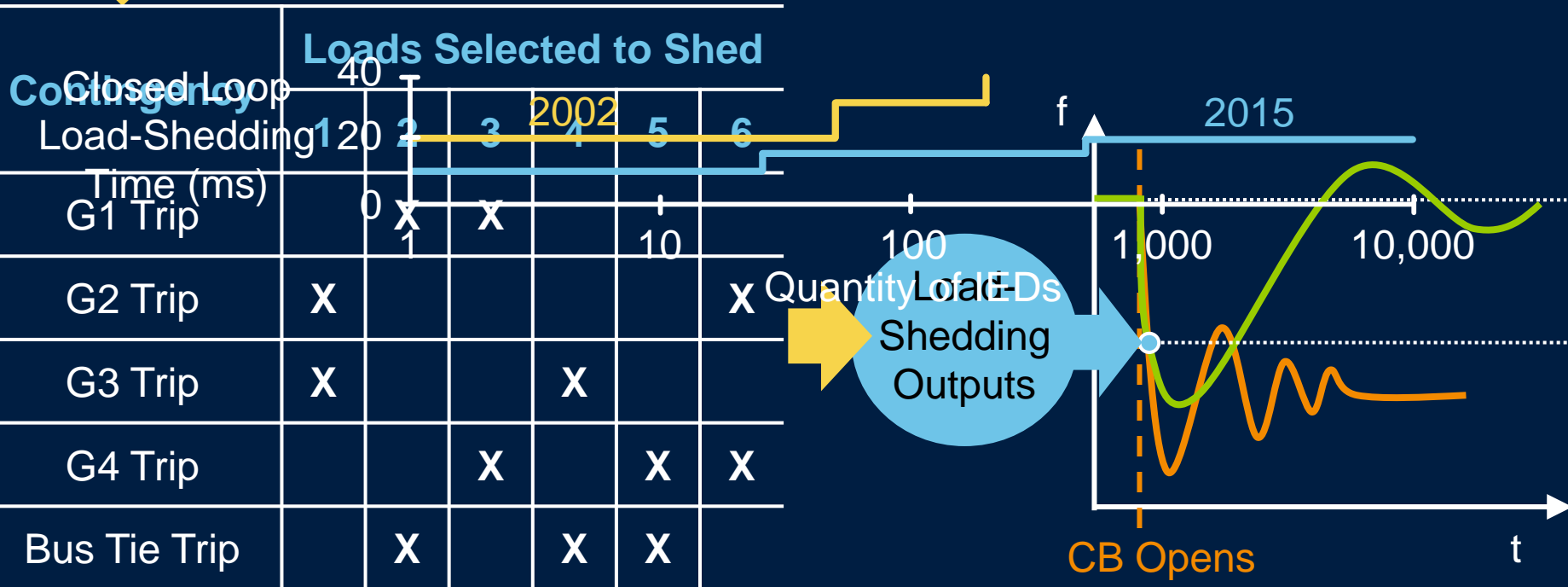
- Front-end processing facilitates scaled architecture and *subcycle* communications
- Crosspoint switch enables *subcycle* load shedding
- *Subcycle* load shedding allows seamless islanding

2002 – Motor Oil Hellas

Lessons Learned

Trigger Inputs

Crosspoint Switch



Plant 1
(230 kV GIS)

2006 - Saudi Aramco

Shaybah, Saudi Arabia

Plant 2
(230 kV GIS)

Plant 2
(115 kV GIS)

Plant 3
(69 kV AIS)



2006 – Saudi Aramco

Factory Acceptance Tests Improved With Hardware-in-the-Loop Testing



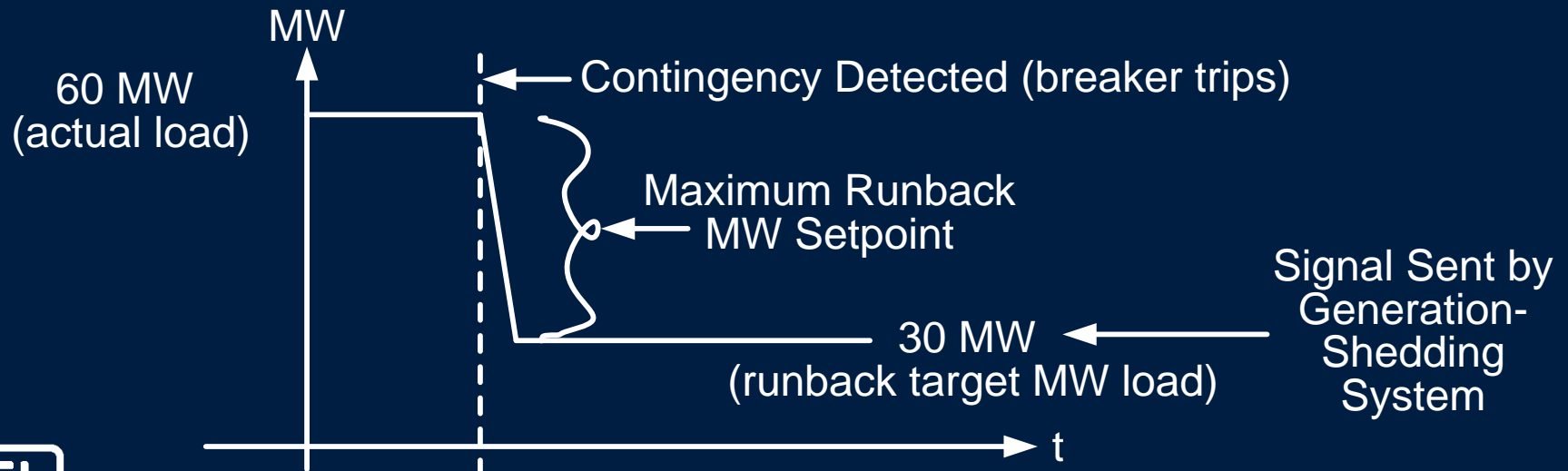
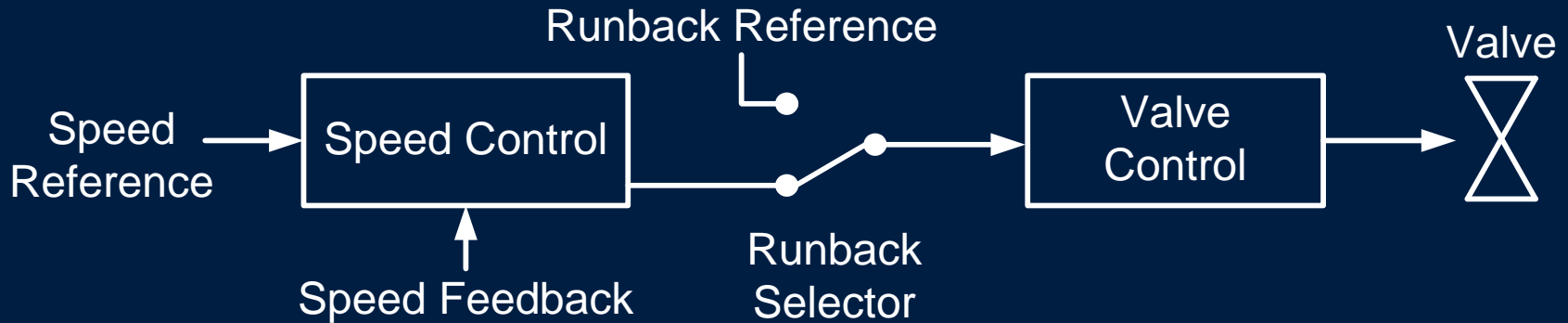
Status

Dynamic
Simulation

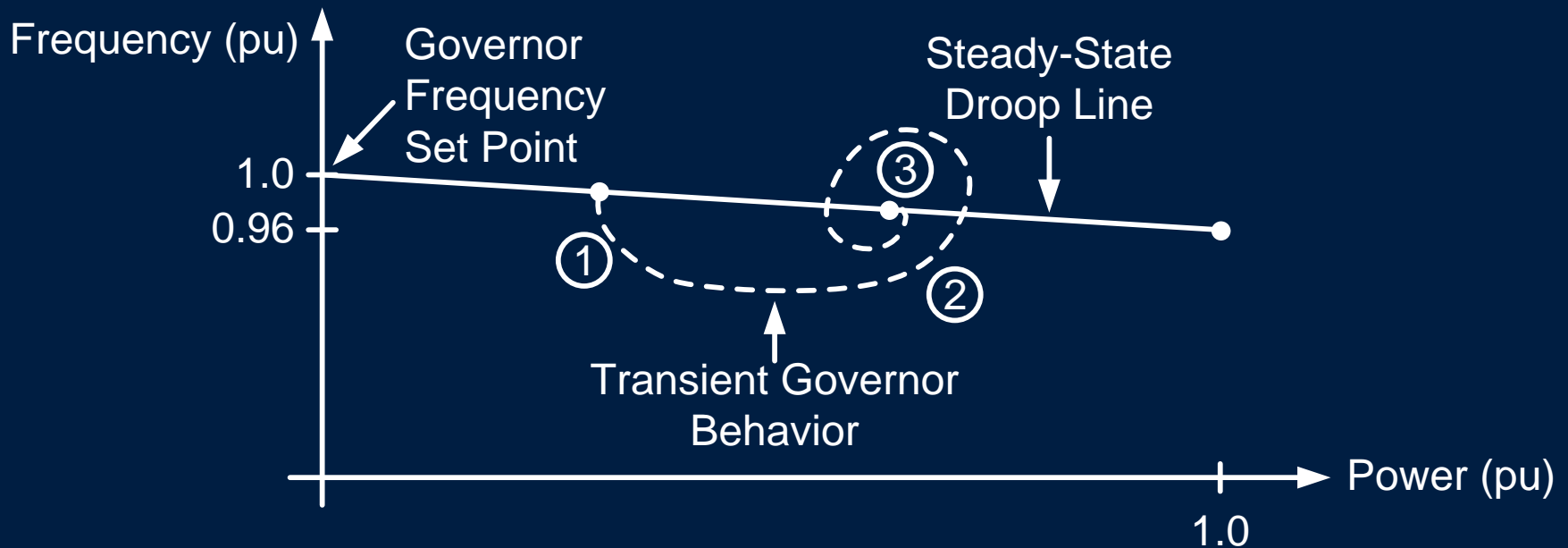


Generation Runback

Making Turbine Respond at Speed of Inverter



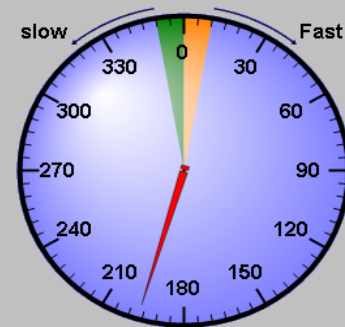
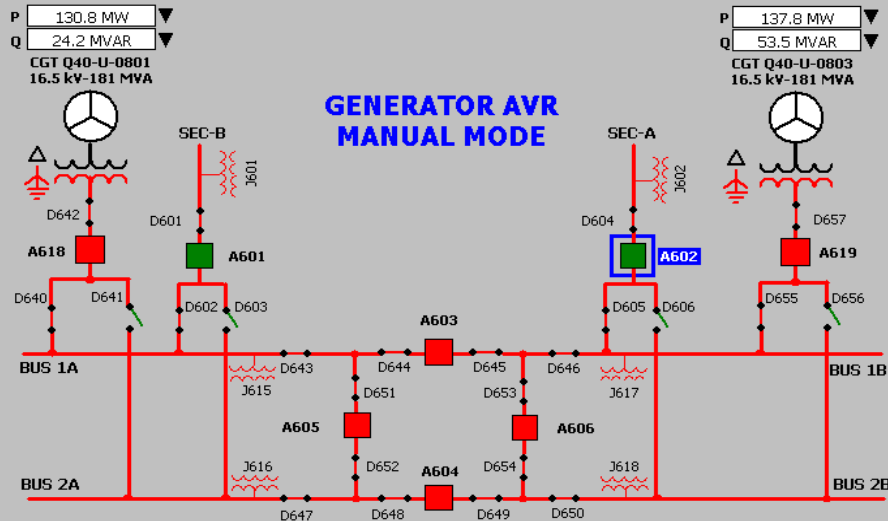
Dynamic Behavior Requires Modeling Mechanical *and* Electrical Systems



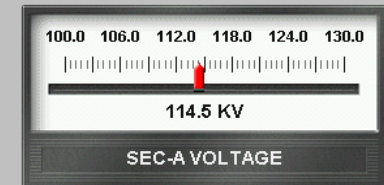
System Synchronization

Safely Reconnecting Islanded Grids

BACK SYNCHRONIZATION



SYNCHROSCOPE



BSR-A

| | |
|------------------|----------|
| BUS 1B FREQUENCY | 60 HZ |
| SEC-A FREQUENCY | 60 HZ |
| SLIP FREQUENCY | 0 |
| ANGLE DIFFERENCE | 197 |
| BUS 1B VOLTAGE | 113.5 KV |
| SEC-A VOLTAGE | 114.5 KV |

| | | | |
|--|--|------------------------------------|--|
| <input checked="" type="radio"/> ENABLED | <input type="radio"/> TRIP | <input type="radio"/> Target Reset | |
| <input type="radio"/> SYNCH SUCCESSFUL | <input type="radio"/> CLOSE FAILED | <input type="radio"/> SELECT CB601 | <input type="radio"/> ABORT SYNCH PROCESS |
| <input type="radio"/> FREQ. OK TO INITIATE | <input type="radio"/> VOLT. OK TO INITIATE | <input type="radio"/> SELECT CB602 | <input type="radio"/> INITIATE SYNCH PROCESS |
| <input type="radio"/> SLIP OK | <input type="radio"/> VOLT. DIFF. OK | <input type="radio"/> SELECT CB603 | <input type="radio"/> CLOSE SELECTED CB |
| <input type="radio"/> dF/dT OK | <input type="radio"/> dV/dT OK | <input type="radio"/> SELECT CB604 | <input type="radio"/> AUTO LOCAL |
| <input type="radio"/> ANGLE OK | <input type="radio"/> SELECTED CB OPEN | <input type="radio"/> SELECT CB605 | <input type="radio"/> AUTO REMOTE |
| <input type="radio"/> MASTER | <input type="radio"/> BREAKER STATUS ALARM | <input type="radio"/> SELECT CB606 | <input type="radio"/> LOCAL MANUAL |
| <input type="radio"/> REQUEST UNAVAILABLE | <input type="radio"/> CLOSE LOCKOUT | | |
| <input type="radio"/> GEN. FREQ. HI | <input type="radio"/> SYNCH COMM. ALARM | | |
| <input type="radio"/> GEN. FREQ. LO | <input type="radio"/> VOLT. HI | | |
| <input type="radio"/> RAISE GEN. FREQUENCY | <input type="radio"/> VOLT. LO | | |
| <input type="radio"/> LOWER GEN. FREQUENCY | <input type="radio"/> RAISE VOLT. | | |
| | <input type="radio"/> LOWER VOLT. | | |

SEL

Graphical Interfaces

Teach Operators to Dispatch Grid Differently

| Contingency | # | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
|-------------------|----|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|--|
| NGL BC B721 | 1 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL BC B723 | 2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL BC B722 | 3 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL BC B720 | 4 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 BC B712 | 5 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 BC B714 | 6 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 BC B713 | 7 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 BC B711 | 8 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 BC B612 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-2 BC B505 | 10 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL/G4 Tie A | 11 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL/G4 Tie B | 12 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 Intertie A | 13 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 Intertie B | 14 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-4 GOSP-2 Tie | 15 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL/GOSP-3 Tie A | 16 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| NGL/GOSP-3 Tie B | 17 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-3 BC B701 | 18 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-3 BC B702 | 19 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |
| GOSP-3 BC B703 | 20 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | |

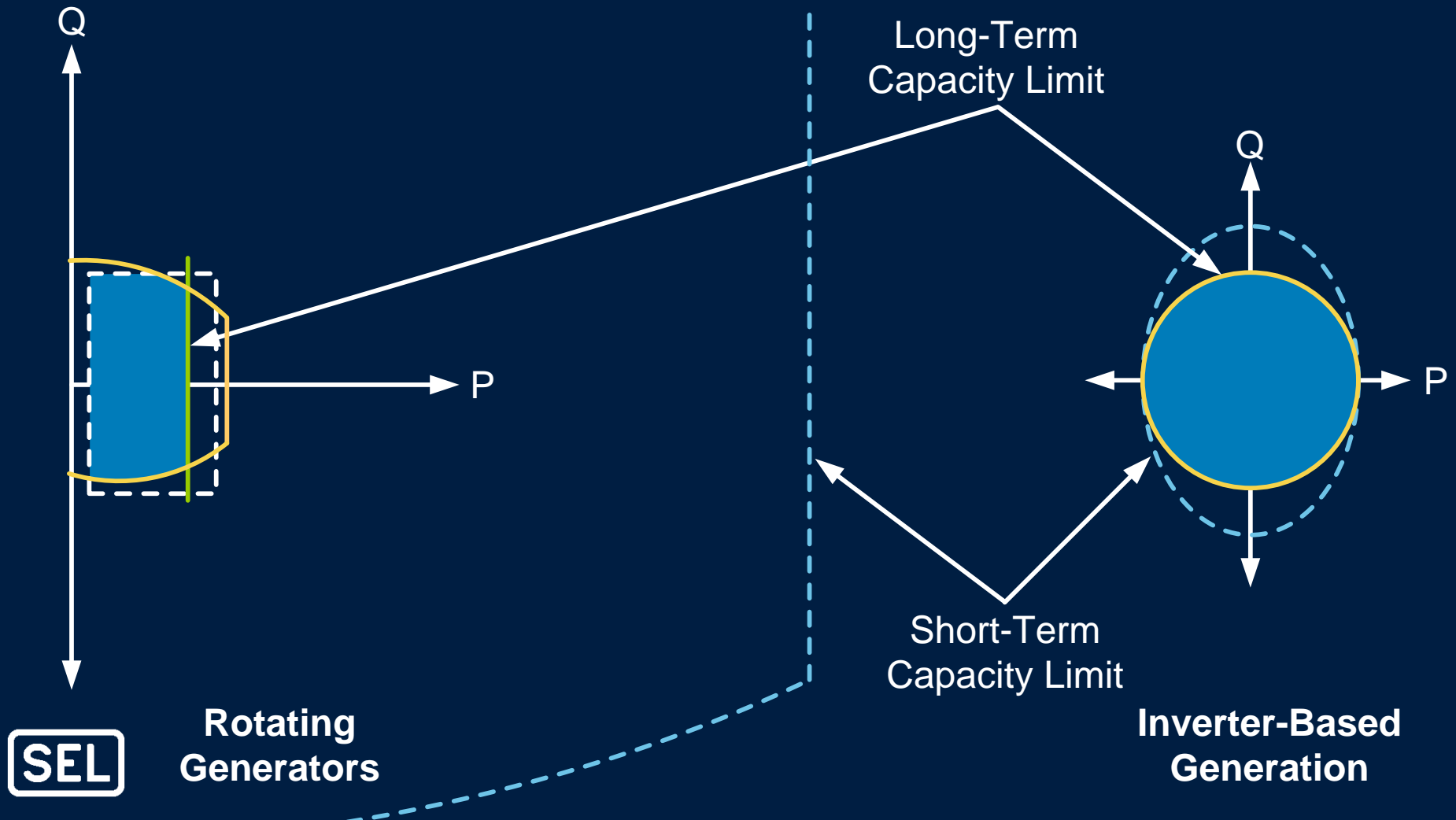
2008 – Presidio, Texas

4 MW NaS Battery Microgrid Controls



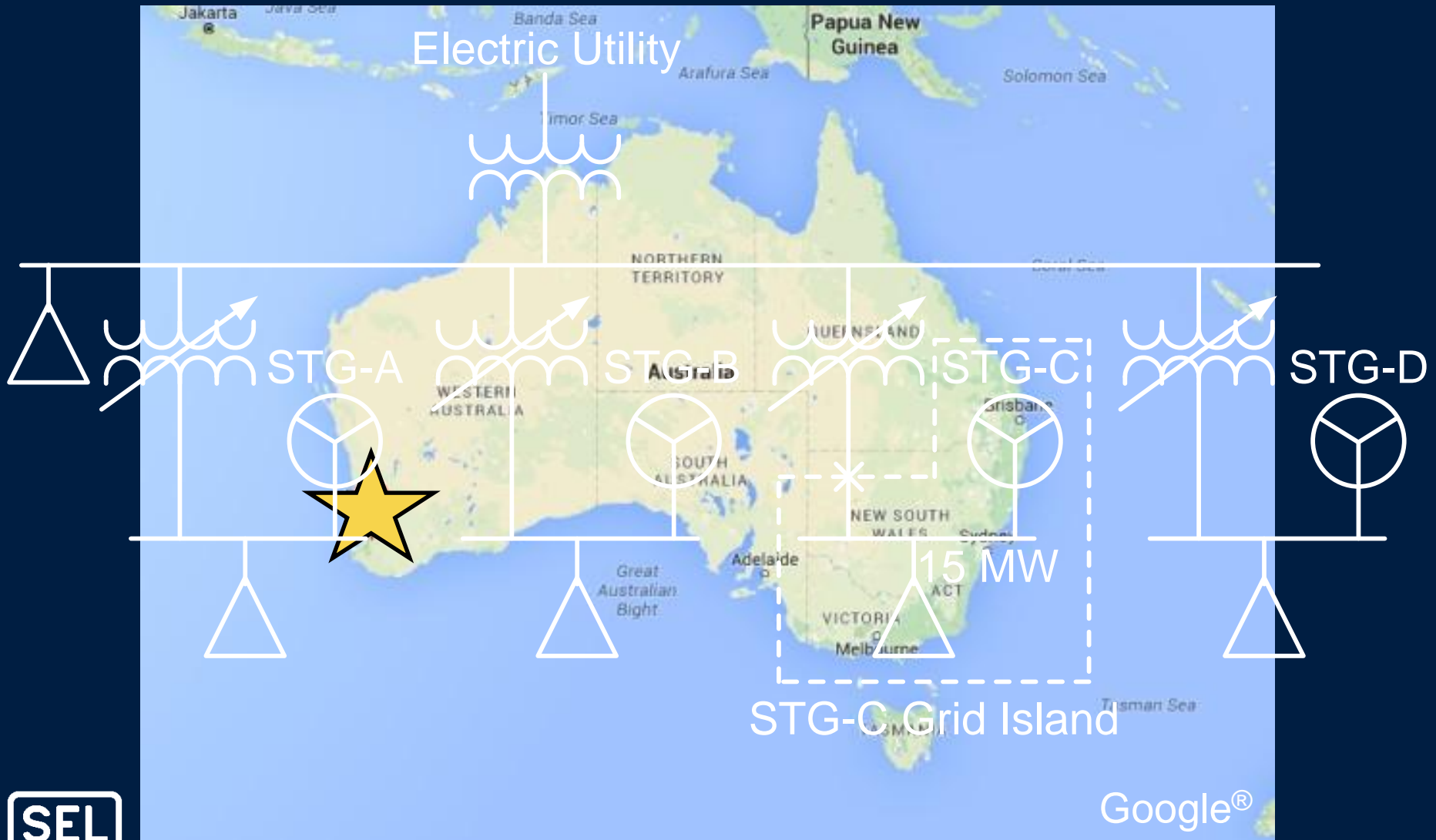
2008 – Presidio, Texas

Inverters Are Not as Robust as Rotating Machinery

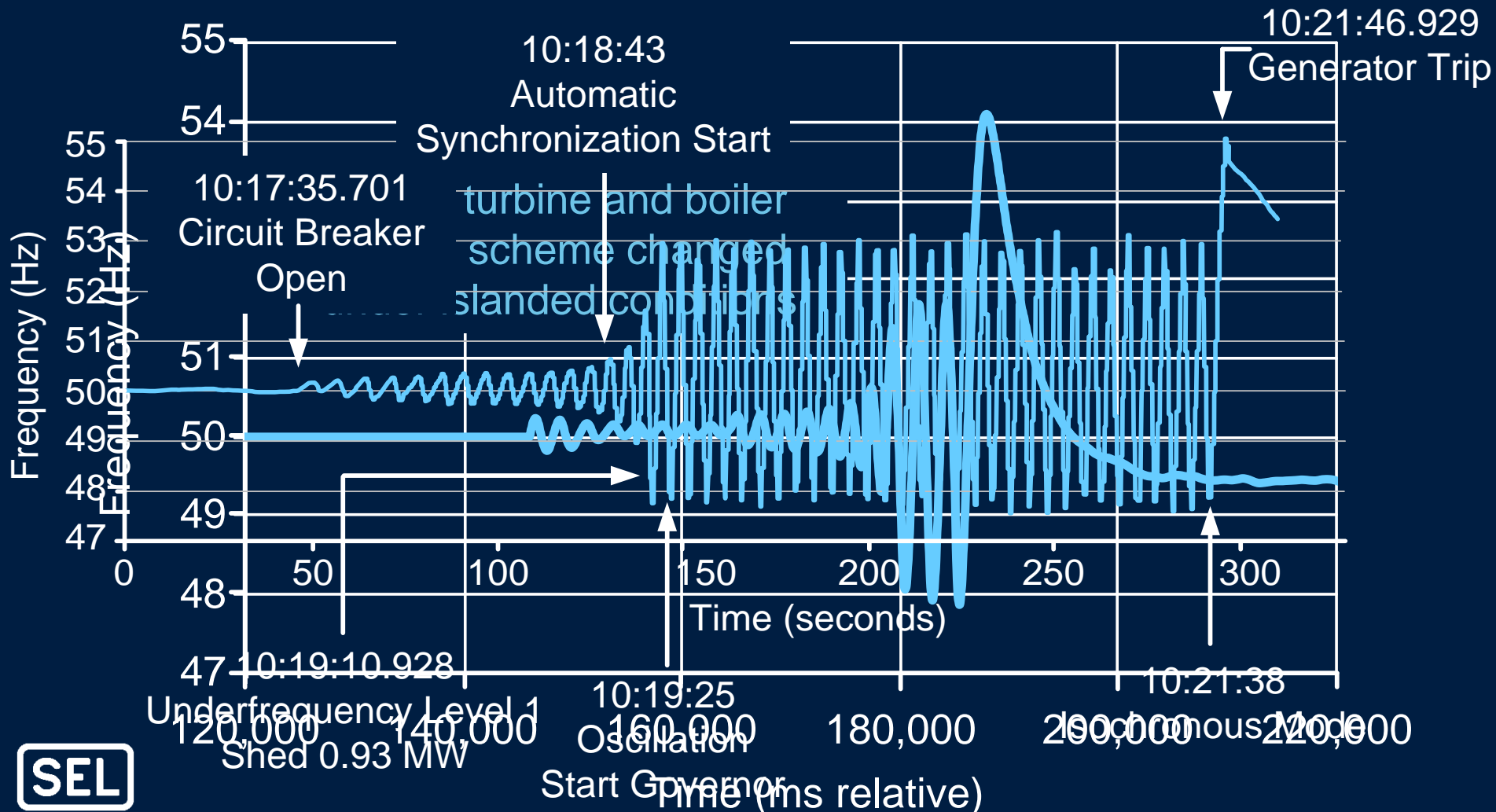


2010 – BHP Worsley Alumina

Collie, Australia

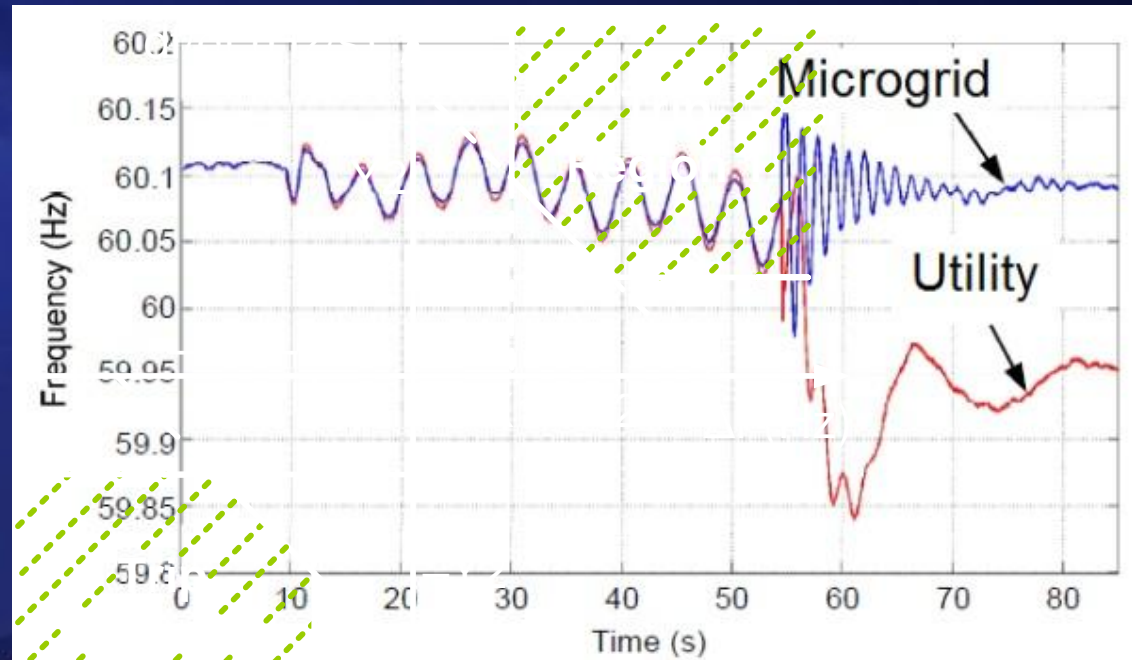


Islanded Steam Turbines and Electronic Loads May Not Mix!



2010 – BHP Worsley Alumina

Intentional Disconnecting at PCC Increases Reliability



2012 – Chevron Jack and St. Malo Offshore Platforms

In-Depth Complexity Security Required!

Layer 3.5 – Business Networks

Sealed Down for Remote Facility

Physical Security Perimeter

Layer 3.5 – DMZ

Firewalls

Thin Clients

Firewalls

Layer 3 – Visualization

Local
Visualization

Engineering
Applications

Layer 2 – Controls

Firewalls

Microgrid Controller

Layer 1 – Protection

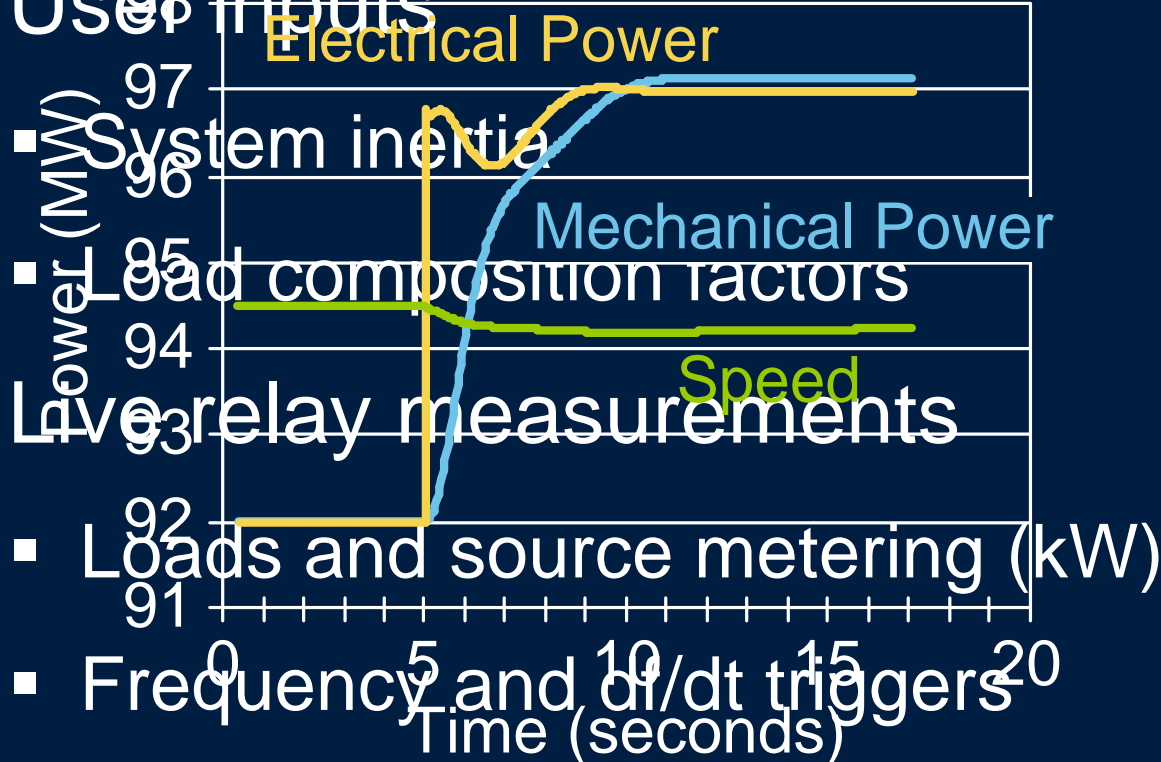
Protective
Relays

IO modules

Inertia Compensation and Load Tracking (ICLT)

Balances Power Mismatch for Underfrequency Events!

- Use 8 inputs

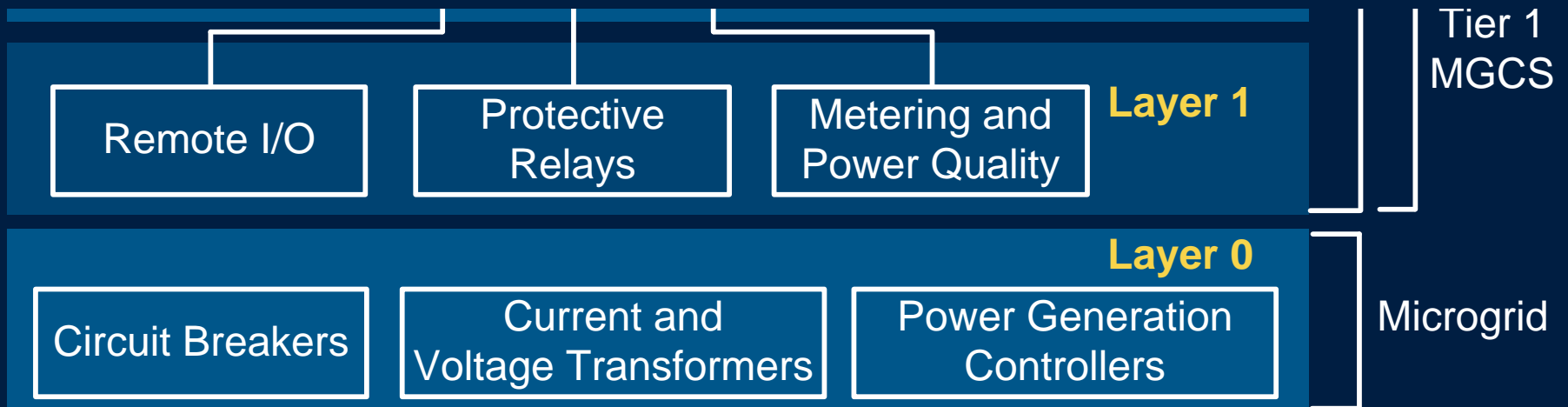


2014 – University of California

San Diego, California



Industrial and utility technology, procedures, modeling, testing, and commissioning methods were a perfect fit!



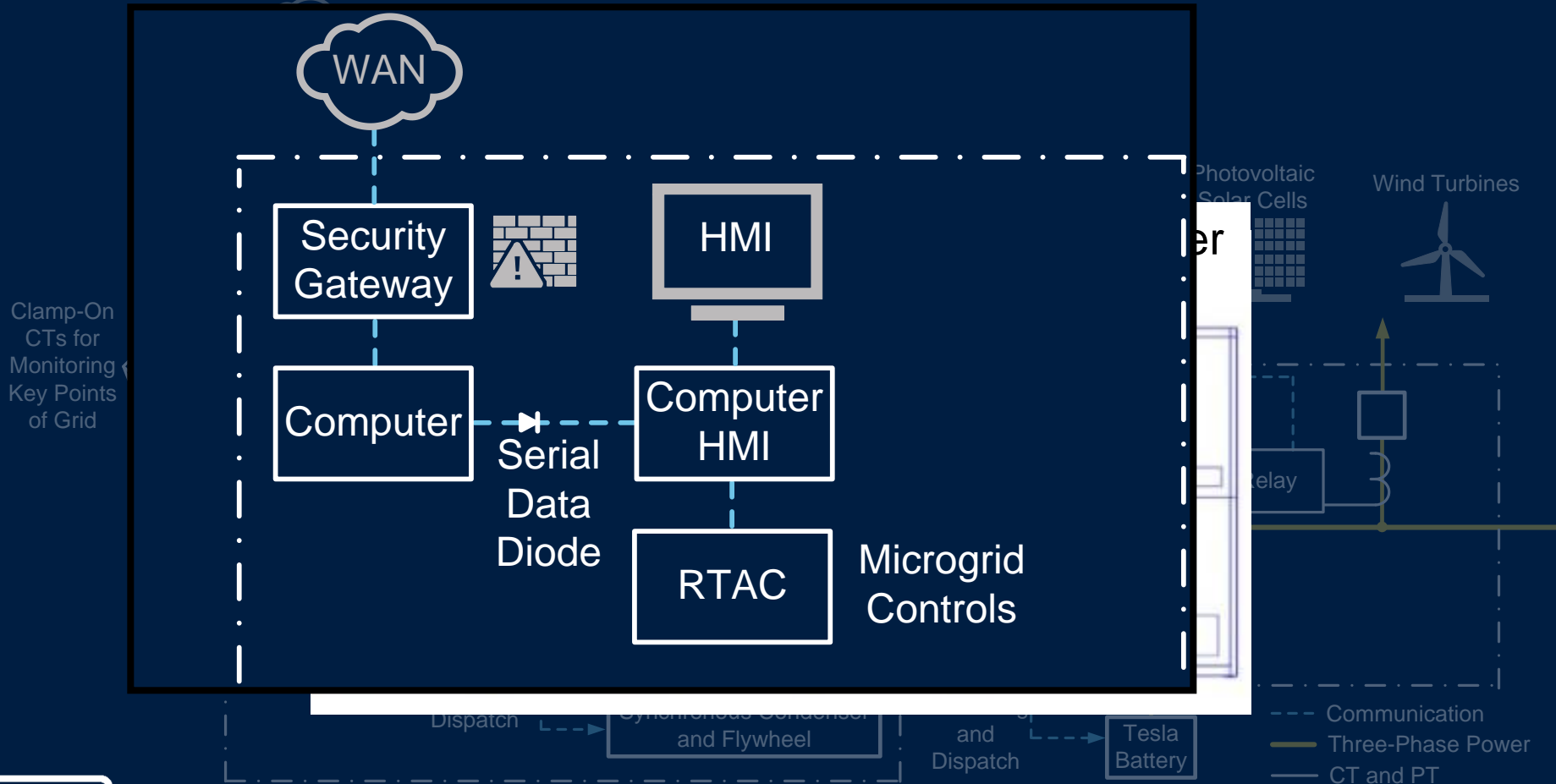
2015 – Borrego Microgrid 2.0

PCC Is Protection Challenge

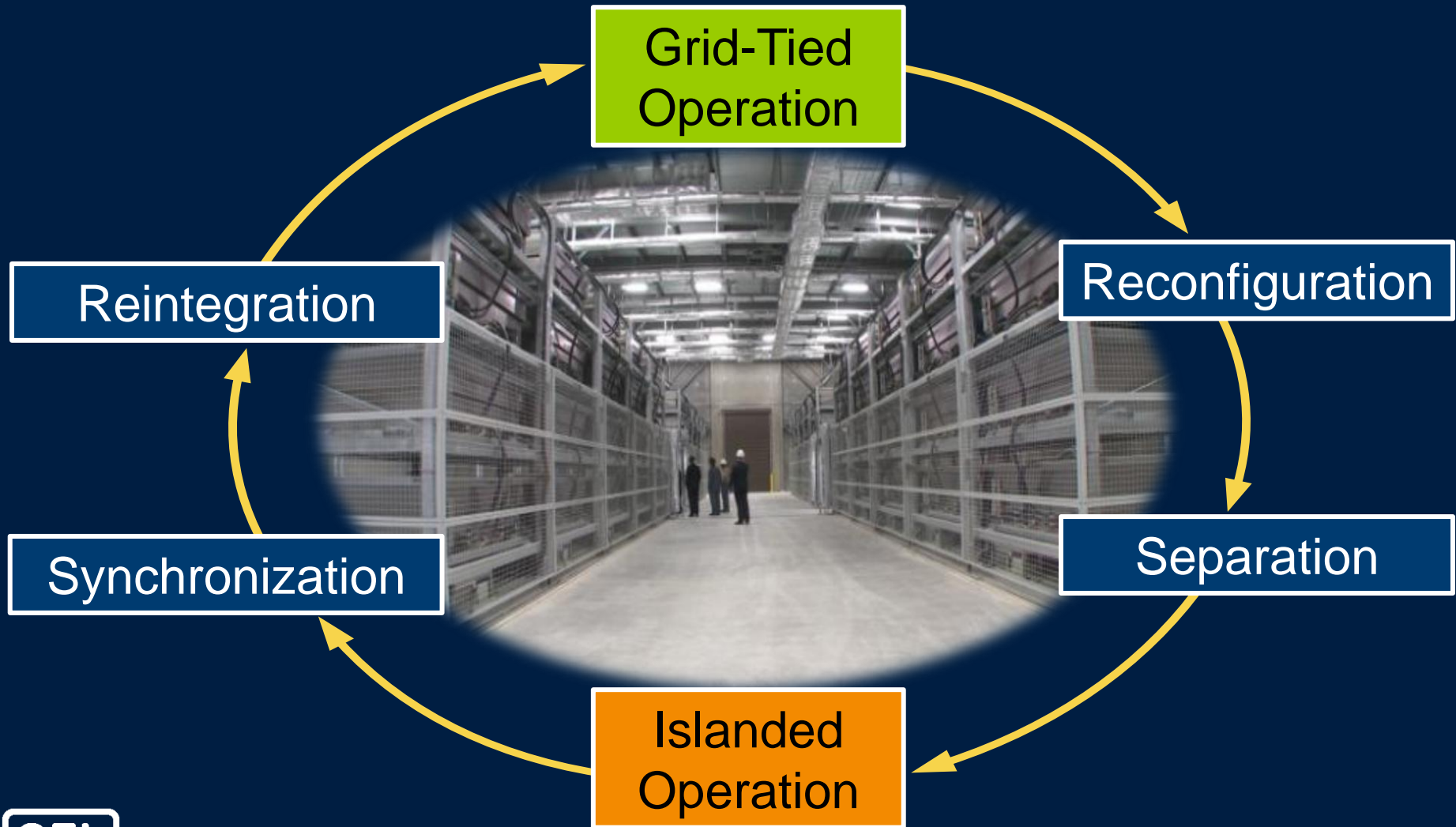


2016 – Navy Seabees

Microgrid Controls, Protection, and Security Can Be Small and Portable



Modern Microgrids Automatically Separate, Survive, and Synchronize



Questions?



References

- [1] E. R. Hamilton, J. Undrill, P. S. Hamer, and S. Manson, "Considerations for Generation in an Islanded Operation," proceedings of the 56th Annual Petroleum and Chemical Industry Conference, Anaheim, CA, September 2009.
- [2] A. Al-Mulla, K. Garg, S. Manson, and A. El-Hamaky, "Case Study: A Dual-Primary Redundant Automatic Decoupling System for a Critical Petrochemical Process," proceedings of the 6th Annual Petroleum & Chemical Industry Committee Europe Conference, Barcelona, Spain, May 2009.
- [3] S. Manson, A. Upreti, and M. J. Thompson, "Case Study: Smart Automatic Synchronization in Islanded Power Systems," proceedings of the Power and Energy Automation Conference, Spokane, WA, March 2013.
- [4] S. Manson, A. Khatib, M. Checksfield, and P. Duffield, "Case Study: Simultaneous Optimization of Electrical Grid Stability and Steam Production," proceedings of the 61st Annual Petroleum and Chemical Industry Technical Conference, San Francisco, CA, September 2014.
- [5] S. Manson, G. Zweigle, and V. Yedidi, "Case Study: An Adaptive Underfrequency Load-Shedding System," proceedings of the 60th Annual Petroleum and Chemical Industry Technical Conference, Chicago, IL, September 2013.
- [6] S. Manson, B. Kennedy, M. Checksfield, "Solving Turbine Governor Instability at Low Load Conditions," proceedings of the 62nd Annual Petroleum and Chemical Industry Technical Conference, Houston, TX, October 2015.